

Hochschule für Technik und Wirtschaft Berlin

University of Applied Sciences





German Grid Code Compliance Assessment Practice

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htu. Germany's transition to renewable electricity generation

- Rapidly increasing share of renewable energy sources (RES) in total installed capacity and generation
 - around 50% of gross electricity consumption in 2022
 - mostly inverter based resources (wind and solar)
 - Substituting coal and gas based conventional power plants

With RES goal of at least 80% in electricity generation by 2030

RES must verifiably be capable of providing:

- Frequency stability
- Voltage stability
- Ride-through capability
- Capability to survive systems splits / islanding (new!)

in an inverter based resources dominated grid

with little remaining synchronous generation for extended periods of time

htu. Germany's approach to Grid code compliance verification



¹FGW e.V. – Fördergesellschaft Windenergie und andere Dezentrale Energien

Government supported 3rd party verification & certification

- Verification of compliance with grid codes and government RES grid support incentives
- Independence, impartiality, transparency
- Competency and quality verified by accreditation
- Risk reduction for manufacturers, plant developers/operators and TSO/DSO
- Reduction of interconnection process times and costs

htu. FGW 3-Step Compliance Assessment Process

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htu. Conformity assessment Power Generation Unit



duration: 6 - 12 month \$23 ESIG Fall Technic 的 如果 中国 Pall The Philipper Morkshop

htu. Broad range of assessment methods for plant certification

The **unit certificate** as a basis for plant assessments:

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Mark Meuser: Grid code compliance verification acc. TR8. Approach Rationale Experiences. Presentation at IEEE P2008.2 WG. FGH Zertifizierungsgesellschaft mbH. April 2023.

htu. Grid Fault Measurement according to FGW und IEC

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Example: Voltage Dip



Standardized procedures / quantitative approach: detailed and aggregated plant model

Detailed plant model – need for grid connection approval

- Most grid code requirements apply to the plant connection point
- Model based on validated unit models. Plant controller and compensation need separate validated models.
- Grid code requirements and plausibility checks are performed.
- No comparison to measurements at plant level.

Aggregated Plant Models – for system studies (can be demanded by grid operator, but not used so far)

- Based on unit model.
- All evaluations are at the plant connection point
- Active and reactive power reference changes
 - Response to voltage and frequency changes, protection
 - Comparison to detailed (validated) plant simulation model (100 ms step size + 10 sec moving average filter)
- Balanced and unbalanced FRT
 - Response to voltage dips

htu. Emerging requirements and use of EMT-Models

- For long, FGW TG4 required only RMS-Models.
 - Registry of FGW Certificates available at: <u>https://wind-fgw.de/database/?lang=en</u>
- In the latest release of TG4 (V10), EMT-Models have been added.
- EMT-Models are required:
 - ▶ If RMS-Model are not valid for short circuit ratios < e.g. 3
 - SCR-Ratio will decrease open issue!
 - For offshore wind plants connected via HVDC
 - For locations of wind plants close to HVDC-stations
 - For the evaluation of frequencies above 5 Hz (if needed)

Differences to U.S. approach:

- Evaluation of negative sequence protection settings uses negative sequence RMS models
- Evaluation of negative sequence could be based on negative sequence loadflow-models as well

htu. Backup Slides

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htu. Standardized procedures / quantitative approach: limitations

Standardized procedures + quantitative approach

- Aims to provide transparent and comparable criteria for evaluation
- Cost and time efficient, allows automated evaluation
- De-risking for manufacturer, plant operator & TSO/DS=

Limitations

- Definition of "transient" areas that can be excluded due to limitations of the applied positive sequence (RMS) models to some extent arbitrary
- Model limitations
 - Fault currents difficult to model especially for DFIG- Turbines
 - Transformer saturation not handled by RMS-models
 - Post-fault active power recovery can be impacted by wind speed changes -> some expert opinion necessary
 - Post-fault active power changes due to eigenfrequency of drive train are difficult to model accurately (depends on pitch angle, fault conditions,...)

htu. Different Focus of RMS and EMT-Models WECC - FGW

Joint Work in WECC 2nd generation models and IEC 61400-27

- Generic models available from WECC and IEC
- Manufacturer specific positive (and negative) sequence models usually used in Germany

Different focus of RMS models WECC/IEEE and FGW/IEC

WECC /USA:

- slightly simpler version of the models for system studies
- measurement of operating plants, evaluation of fault events
- Validation based on <u>expert opinion</u>

IEC/Europe:

- slightly more detailed models for <u>connection studies</u>, <u>model validation based on</u> <u>measurement</u>
- measurement of FRT-tests of unit
- Validation based on <u>standardized procedures</u> (unit model only, no validation of plant model)
- Plant Model based on validated unit model, for connection studies

Different focus of EMT models WECC/IEEE and FGW

- IEEE 2800/.2: Paradigm change in U.S. towards more plant conformity assessment using models
- ▶ WECC: negative sequence evaluation for connection studies
- ▶ FWG: connection studies for HVDC-connected units

htu. Standardized procedures / quantitive approach: unit models

Unit models

 All evaluations at the turbine terminals (LV or MV at manufacturers choice). Some grid code requirements - like reactive current ramp rates during FRT - apply to the unit terminals.

Unit models - normal operation

- Active and reactive power capability diagram (PQ)
 - Comparison to measurements, (steady state)
- Active and reactive power reference changes
 - Comparison to measurements (<10ms + 15 sec moving average)
 - Different acceptance criteria for transient periods and steady state operation
- Response to frequency changes
 - Comparison to measurements (internal frequency ref. change)

Unit models – FRT

- Active and reactive current response to voltage dips
- balanced & unbalanced faults, evaluation of positive & negative sequence currents.
 - Comparison to measurements (<10ms + 15 sec moving average)

FGW TG4 & IEC 61400-27-1 Positive and negative sequence representation

In order to compare measurement and simulation, the positive (and if required: negative) sequence of measurement values (voltage, current) is compared to the equivalent (filtered) RMS simulation value.



German Validation Standard FGW TG4: transient and stationary periods

Voltage dip, example of voltage, reactive power and active power 90% Measurement IVAI */t Simulation tansient tationary ansien ationarv ransien C3 C1 r B1 r B2_r C2 r onary stationary transient transien B2 a B1 a C1 a C3 C2 a

The measured event is divided into transient and stationary periods

Note that IEEE P2800.2 is currently not aiming for quantitative pass/fail criteria - but engineering judgement.

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Validation Example: balanced fault 1. comparing measurement and simulation

- Comparison of measurement and simulation of reactive currents of a balanced voltage dip down to 45 % rated voltage.
- The reactive power is changed as the voltage changes.
- Transient periods are highlighted with red color, steady state periods green



Validation Example: balanced fault 2. Calculating averages of transient and stationary ranges

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Calculation of averages for steady state and stationary ranges for measurement (subplot 1) and simulation (subplot 2)



Validation Example: balanced fault 3. Comparison of averages and positive sequence



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- Calculating the difference of
 - average values (subplot1) and
 - positive sequence values (subplot 2)
 - of measurement and simulation (blue) compared to allowed limits (red)

