

Wind Integration

Lessons Learned

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(Murphy's Law Is Alive And Well)

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GENERAL ISSUES



General Wind Location Considerations

- Most of New England Wind Installations Located on Remote Mountain Ridgelines
- Connect Into Weak Transmission System
 - Away from Bulk Transmission Backbone (345 kV in New England)
 - Serving Sparse Loads
 - Never Designed For High Power Transfers
 - Lack of Reactive Resources in These Areas
 - Lack of multiple transmission paths (single outages cause restriction)
 - Low Short Circuit Strength can cause WTG control stability issues



Minimum Interconnection Standard

- This is a tariff requirement imposed by FERC
- Minimum required upgrades, consistent with:
 - No degradation in all-lines-in-service transfer capability
 - All reliability standards must be met
 - ISO can still operate and maintain the system reliably
 - Maximum one-for-one displacement of existing/proposed generation
- Minimum Interconnection Standard
 - Does not ensure incremental transmission capacity to serve load
 - Does ensure no degradation to load-serving capability of the system
 - Consistent with market and Tariff constructs for Network Resources

CASE STUDY ONE



Northern Maine



Keene Road Area

- First proposed wind farm in the area fed by single 115 kV line
 - Low rating, 68 MVA
 - 40 years old at the time, in need of rebuild
 - Serve local paper mill loads in conjunction with mill generation
- Transmission Owner proposed adding 345 kV/115 kV transformation to allow for line rebuild
 - System Impact Study completed in 2008 with proposed 90 MW of wind
 - The area had never been previously assessed for stability issues
 - Transformer tied 115 kV to a +450/-150 Mvar SVC on the 345 kV which in turn is a tie line to neighboring RC (New Brunswick Power)
 - 120 MW existing mill hydro + steam generation with 60 MW mill load

- Inadequate dynamics models for existing 70+ year old mill generators and loads
- In the same timeframe, other wind farms proposed in area
 - Eventually another 142 MW would be built in the area

Keene Road Area

- Plant studied under minimum interconnection standard
- Post-construction issues identified
 - Totally different characteristics with new 345/115 kV transformer
 - Required operating with one 345 kV breaker normally open
 - Created new contingency not previously studied
 - Loss of a 345 kV line now dead-ends the transformer
 - Stability export limit established based on new contingency
 - Not all generation (wind + mill hydro) in the pocket can fit
 - Certain maintenance conditions cause transient high voltage spike
 - Driven by SVC response to remote/high impedance faults
 - Faults weak enough to prevent SVC from blocking
 - Much too fast phenomena for PSSE, so PSCAD study required
- Requires electrical disconnection of wind turbines to avoid overvoltage damage potential

CASE STUDY TWO



Keene Road Area

- Two additional wind plants located in same general area
- Both plants connected under minimum interconnection standard
- Both connected to 115 kV system with poor SCR (<2)
 - Second plant in-service 16 months after first
- Very similar designs
 - Both plants required synchronous condenser (SC) per Planning to mitigate SCR

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- Same SC and wind turbine generator (WTG) manufacturers

Keene Road Area

- First Plant SC reverse power relay issues
 - Unexpected tripping after remote lightning strike
 - Unknown reverse power protection package on SC
 - Intended for anti-islanding
 - Trip of SC intentionally cross-tripped wind far
 - Detailed event reconstruction
 - Worked with manufacturer on proper settings
 - PSCAD analysis required due to WTG model accuracy required for accurate reverse power shape

- Work with same manufacturers on second plant
 - Plant had not yet been fully commissioned
 - Same protection package
 - Showed more severe reverse power spike

CASE STUDY THREE



Northern New Hampshire

- Plant studied under minimum interconnection standard
- Wind Plant located weak 115 kV looped system
 - Poor reactive support and SCR / low rated 115 kV lines (100 to 150 MVA)
 - Area prone to unacceptable transient and steady state voltage performance
- Planning identified need for additional reactive support
- Severely limited during facility out and nearby generator status

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Not only generator status but AVR status as well

Northern New Hampshire

- Based on planning criteria lead/lag turbine capability turbines, static caps and, DVAR adequate for full operation
- Planning did not determine exact details on how reactive elements were to be coordinated resulting controls optimized after plant became operational
 - Plant controller manages lead/lag on turbines, static caps, DVAR
 - Restrictive voltage control bandwidth to respect stability limitations
- Reactive capability found to be problematic under facility out conditions
- Plant significantly restricted for many combinations of facility out conditions (multitude of operating guides for operators)
 - Poor voltage damping during transient timeframe
 - Potential for post-fault LVRT actuation due to weak system
 - Potential for post-fault high voltage trip due to weak system
- Required extensive testing in coordination with developer and manufacturer to tweak Plant Controller to cover myriad of additional system configurations
- Majority of all-lines-in-service restrictions eliminated, still some facility out restrictions

CASE STUDY FOUR



Northern Vermont

- Plant connected under minimum interconnection standard
- Located in a weak system, connected radially to networked 46 kV sub-transmission
 - Very poor reactive support and SCR
- General area also contains HVDC tie to Hydro Quebec as well as existing hydro, other wind and fossil resources
- Resulted in new constrained voltage / stability export limited interface
 - Identified during the interconnection process
- Planning identified synchronous condenser requirement in system upgrades to maintain all-facilities-in-service transfer limits

Northern Vermont

- Plant commercial before SC in-service
 - Resulted in significant MW restriction
- Additional limitations identified under facility out conditions
 - Post-contingent low voltage, post-fault LVRT and high voltage trips, as well as sub transmission network thermal overloads all possible
- To ease some restrictions underlying sub-transmission network consider in analysis
- Eventually SC added which mitigated most restrictions
- Weakness of local system results in significant number (> 20) of facility outages which impact the limits

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HIGH LEVEL CONSIDERATIONS



General Considerations in New England Region

- Minimum interconnect fall-out
- Wind turbine model issues
 - Don't work
 - Changing all the time
 - Black box models hard to debug
 - Proprietary models (intellectual property) create issues between software applications
 - Positive sequence models may not be valid below certain SCR threshold
- Short circuit strength issues
- Very diverse reactive strategies employed
- Reactive capability testing revealed issues with installed reactive upgrades
 - Field test of STATCOM overload capability revealed improperly configured overload capability below design

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• Should consider requiring field testing of all components

General Considerations in New England Region

- LVRT Characteristic creates self-oscillation
 - Plant connected in area with low SCR ~1.7:
 - Plant sees low voltage, enters LVRT
 - LVRT characteristic reduced MW
 - Reduced MW allows voltage to recover and exits LVRT characteristic
 - MW ramp back up
 - Voltage declines again, then re-entering LVRT mode
 - Mitigating this required careful reactive power coordination
- PSSE Model behavior can approximate real system however:
 - Approximations can create the appearance of issues that may be fictitious

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- In other cases can mask issues
- More detail, better documentation improves confidence in models

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Should always consider PSCAD simulation, requires asked for models upfront



